复旦大学力学与工程科学系

2012 ~ 2013 学年第二学期期末考试

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 课程名称:
 连续介质力学基础
 课程代码:
 MECH130105

 开课院系:
 力学与工程科学系
 考试形式:
 开卷/闭卷/课程论文

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Problem 1 (Fundamentals of curvilinear coordinates)

1. To proof the following identity

$$\boldsymbol{\nabla} \times (\boldsymbol{\nabla} \times \boldsymbol{\Phi})^* = \boldsymbol{\nabla} \otimes (\boldsymbol{\Phi} \cdot \boldsymbol{\nabla}) + (\boldsymbol{\nabla} \cdot \boldsymbol{\Phi}) \otimes \boldsymbol{\nabla} - \boldsymbol{\Delta} \boldsymbol{\Phi} - \boldsymbol{\nabla} \otimes (\boldsymbol{\nabla}(tr\boldsymbol{\Phi}))$$
$$- \boldsymbol{I} [\boldsymbol{\nabla} \cdot \boldsymbol{\Phi} \cdot \boldsymbol{\nabla} - \boldsymbol{\Delta}(tr\boldsymbol{\Phi})]$$

for any symmetric affine tensor $\mathbf{\Phi} = \mathbf{\Phi}^* \in \mathscr{T}^2(\mathbb{R}^3)$ through field analysis with respect to general curvilinear coordinates.

2. To consider a tensor represented in two point forms

$$\boldsymbol{\Phi} = \Phi^{i \cdot B \cdot}_{\cdot A \cdot j}(\xi, x) \boldsymbol{g}_i(x) \otimes \boldsymbol{G}^A(\xi) \otimes \boldsymbol{G}_B(\xi) \otimes \boldsymbol{g}^j(x)$$

where $\{\boldsymbol{g}_i(x)\}_{i=1}^m$ are covariant basis with respect to the curvilinear coordinates $X(x) \in \mathscr{C}^p(\mathscr{D}_x, X(\mathscr{D}_x))$ and $\{\boldsymbol{G}_A(x)\}_{A=1}^m$ to $X(\xi) \in \mathscr{C}^p(\mathscr{D}_\xi, X(\mathscr{D}_\xi))$ accompanying with the relations $x = x(\xi) \in \mathscr{C}^p(\mathscr{D}_\xi, \mathscr{D}_x)$. To deduce the representation of $\frac{\partial}{\partial x^l} \boldsymbol{\Phi}(x)$ through covariant differentiations with respect to different curvilinear coordinates.

3. The so-called transfer tensor is defined as

$$\mathbf{I} = g_A^i(\xi, x) \, \mathbf{g}_i(x) \otimes \mathbf{G}^A(\xi), \quad g_A^i := (\mathbf{g}^i, \mathbf{G}_A)_{\mathbb{R}^m}$$

To prove one of the relations

$$\frac{\partial}{\partial\xi^L} \boldsymbol{I}(\xi) = \boldsymbol{0}, \quad \frac{\partial}{\partial x^l} \boldsymbol{I}(x) = \boldsymbol{0}$$

Problem 2 (Stain tensor on an arbitrary deformable surface) Based on the intrinsic decomposition with respect to any direction

$$oldsymbol{\Phi} = \left\{egin{array}{ll} oldsymbol{e}\otimes(oldsymbol{e},oldsymbol{\Phi})_{\mathbb{R}^3} - [oldsymbol{e},[oldsymbol{e},oldsymbol{\Phi}]] \ (oldsymbol{\Phi},oldsymbol{e})_{\mathbb{R}^3}\otimesoldsymbol{e} - [[oldsymbol{\Phi},oldsymbol{e}],oldsymbol{e}] \end{array} egin{array}{ll} orall oldsymbol{e}|_{\mathbb{R}^3} = 1, & orall oldsymbol{\Phi}\in\mathscr{T}^p(\mathbb{R}^3) \ (oldsymbol{\Phi},oldsymbol{e})_{\mathbb{R}^3}\otimesoldsymbol{e} - [[oldsymbol{\Phi},oldsymbol{e}],oldsymbol{e}] \end{array}
ight.$$

the following representation of the strain tensor on an arbitrary deformable surface can be deduced

$$\begin{split} \boldsymbol{D} &\triangleq \frac{1}{2} (\boldsymbol{V} \otimes \boldsymbol{\nabla} + \boldsymbol{\nabla} \otimes \boldsymbol{V}) \\ &= \left(\boldsymbol{\theta} - \overset{\Sigma}{\boldsymbol{\nabla}} \cdot \boldsymbol{V} \right) \boldsymbol{n} \otimes \boldsymbol{n} + \frac{1}{2} [(\boldsymbol{\omega} + \boldsymbol{W}) \times \boldsymbol{n}] \otimes \boldsymbol{n} + \frac{1}{2} \boldsymbol{n} \otimes [(\boldsymbol{\omega} + \boldsymbol{W}) \times \boldsymbol{n}] + \overset{\Sigma}{\boldsymbol{D}} \\ & \text{where } \overset{\Sigma}{\boldsymbol{D}} \triangleq \left(\boldsymbol{V} \otimes \overset{\Sigma}{\boldsymbol{\nabla}} + \overset{\Sigma}{\boldsymbol{\nabla}} \otimes \boldsymbol{V} \right) / 2 \text{ is the strain of the boundary, } \boldsymbol{W} := -\left(\overset{\Sigma}{\boldsymbol{\nabla}} V^3 + \boldsymbol{V} \cdot \boldsymbol{K} \right) \times \boldsymbol{n} \\ & \text{is purely determined by the boundary, and } \boldsymbol{\theta} := \boldsymbol{\nabla} \cdot \boldsymbol{V} \text{ is the dilation.} \end{split}$$

- 1. To give the relation between the full dimensional gradient operator $\nabla \triangleq i_{\alpha} \frac{\partial}{\partial X^{\alpha}}$ and the surface gradient operator $\stackrel{\Sigma}{\nabla} \triangleq g^l \frac{\partial}{\partial x_{\Sigma}^l}$. The reason should be indicated.
- 2. To proof the following identity

$$oldsymbol{V}\otimesoldsymbol{
abla}=\left(heta-oldsymbol{
abla}\cdotoldsymbol{V}
ight)oldsymbol{n}\otimesoldsymbol{n}+(oldsymbol{\omega} imesoldsymbol{n})\otimesoldsymbol{n}+(oldsymbol{W} imesoldsymbol{n})\otimesoldsymbol{n}-[[oldsymbol{V}\otimesoldsymbol{
abla},oldsymbol{n}],oldsymbol{n}]$$

3. To fulfill the deduction.

where

4. To give the component matrix of D on a sphere which does the radical oscillation with fixed amplitude and frequency.

Problem 3 (Some studies based on the intrinsic Stokes formulas) We have attained the Stokes formula of the following forms

$$\oint_{C} \boldsymbol{\tau} \circ -\boldsymbol{\Phi} \, dl = \int_{\Sigma} \left(\boldsymbol{n} \times \boldsymbol{\nabla} \right) \circ -\boldsymbol{\Phi} \, d\sigma$$
$$\oint_{C} \left(\boldsymbol{\tau} \times \boldsymbol{n} \right) \circ -\boldsymbol{\Phi} \, dl = \int_{\Sigma} \left(\boldsymbol{\nabla} \circ -\boldsymbol{\Phi} + H\boldsymbol{n} \circ -\boldsymbol{\Phi} \right) \, d\sigma$$

which are termed as the intrinsic Stokes formulas.

1. On any deformable smooth surface, the following identity is keeping valid

$$\left(\boldsymbol{n}\times \boldsymbol{\nabla}^{\Sigma}\right) \cdot \left(\boldsymbol{n}\times \boldsymbol{\Phi}\right) = \boldsymbol{\nabla} \cdot \boldsymbol{\Phi} + H\boldsymbol{n}\cdot \boldsymbol{\Phi}, \quad \forall \, \boldsymbol{\Phi} \in \mathscr{T}^p(\mathbb{R}^3)$$

To prove the identity as mentioned above by the intrinsic Stokes formula of the second kind.

- 2. To deduce the differential equation of mass conservation for the two dimensional compressible steady flow on an arbitrary fixed smooth surface.
- 3. To give the differential equation of mass conservation in detail for the two dimensional compressible steady flow on a fixed sphere.

Problem 4 (Governing equations in Lagrangian variables) The governing equations of continuum media represented in Lagrangian arguments could be listed as follows

$$mass \ conservation \qquad \rho(\xi,t) \, |\mathbf{F}|(\xi,t) = \stackrel{\circ}{\rho}(\xi), \quad \mathbf{F} \triangleq \frac{\partial x^{i}}{\partial \xi^{A}}(\xi,t) \mathbf{g}_{i}(x,t) \otimes \mathbf{G}^{A}(\xi)$$
$$momentum \ conservation \qquad \stackrel{\circ}{\rho}(\xi) \, \mathbf{a}(\xi,t) = \stackrel{\circ}{\rho}(\xi) \, \mathbf{f}_{m}(\xi,t) + \begin{cases} [\mathbf{t} \cdot (|\mathbf{F}|\mathbf{F}^{-*})] \cdot \stackrel{\circ}{\Box} =: \tau \cdot \stackrel{\circ}{\Box} \\ (\mathbf{F} \cdot \mathbf{T}) \cdot \stackrel{\circ}{\Box}, \quad \mathbf{T} = \mathbf{F}^{-1} \cdot \tau \end{cases}$$
$$constitution \ relation \qquad \mathbf{T} = -p \stackrel{\circ}{\mathbf{C}}^{-1} + 2 \left[\frac{\partial \Sigma}{\partial I_{1}} \, \mathbf{I} + \frac{\partial \Sigma}{\partial I_{2}} \, (I_{1} \, \mathbf{I} - \stackrel{\circ}{\mathbf{C}}^{-1}) \right], \quad \stackrel{\circ}{\mathbf{C}} := \mathbf{F}^{*} \cdot \mathbf{F}$$

where the constitution relation is corresponding to the incompressible flow.

The procedure to study the finite bending deflection of cube can be divided into following steps.

1. Configurations and curvilinear coordinates The curvilinear coordinates with respect to the initial physical configuration can be just Cartesian coordinates, namely

$$\xi = \begin{bmatrix} \overset{\circ}{X} \\ \overset{\circ}{Y} \\ \overset{\circ}{Z} \end{bmatrix} \mapsto \overset{\circ}{X}(\xi) = \begin{bmatrix} \overset{\circ}{X} \\ \overset{\circ}{Y} \\ \overset{\circ}{Z} \end{bmatrix} \triangleq \begin{bmatrix} \overset{\circ}{X} \\ \overset{\circ}{Y} \\ \overset{\circ}{Z} \end{bmatrix}$$

The curvilinear coordinates with respect to the current physical configuration is familiar cylindrical coordinates, namely

$$x = \begin{bmatrix} r \\ \theta \\ z \end{bmatrix} \mapsto X(x) = \begin{bmatrix} x \\ y \\ z \end{bmatrix} \triangleq \begin{bmatrix} r\cos\theta \\ r\sin\theta \\ z \end{bmatrix}$$

2. Assumption of deformation One can assume the deformation in the following form

$$\xi = \begin{bmatrix} \overset{\circ}{X} \\ \overset{\circ}{Y} \\ \overset{\circ}{Z} \end{bmatrix} \mapsto x(\xi) = \begin{bmatrix} r \\ \theta \\ \phi \end{bmatrix} \triangleq \begin{bmatrix} r(\overset{\circ}{X}) \\ \theta(\overset{\circ}{Y}) \\ z(\overset{\circ}{Z}) \end{bmatrix}$$

- 3. **Deformation gradient tensor** To calculate the component matrix of deformation gradient tensor **F** with respect to the anholonomic orthonormal bases.
- Strain tensor To calculate the component matrices of strain tensor C with respect to the anholonomic orthonormal bases. Subsequently, its principle invariants can be determined readily.
- 5. **Piola-Kirchhoff stress tensor** To calculate the component matrices of Piola-Kirchhoff stress tensor of the second kind with respect to the anholonomic orthonormal bases.
- 6. Momentum Equation To calculate the component equations of the momentum conservation.

The questions are

- 1. To deduce the component matrix of deformation gradient tensor **F** with respect to the anholonomic orthonormal bases.
- 2. To deduce the component matrix of strain tensor $\overset{\circ}{\mathbf{C}}$ with respect to the anholonomic orthonormal bases.
- 3. To deduce the representations of the principle invariants of $\overset{\circ}{\mathbf{C}}$.
- 4. To deduce the component matrix of Piola-Kirchhoff stress tensor of the second kind **T** with respect to the anholonomic orthonormal bases.
- 5. To deduce all of the component equations of the momentum conservations with respect to the anholonomic orthonormal bases.
- 6. To show that there exists the relation p = p(X), in other words one has $\frac{\partial p}{\partial X} = \frac{\partial p}{\partial Z} = 0$

Note: To give the deduction and calculation in detail. And as the score is considered, the reflection of the correct methodologies is oriented.